

# Lowest PAPR Selection Technique from SLM and PTS with One IFFT Block in Wireless MC-CDMA Communication Systems

Mesri Mokhtaria, Merah Hocine, and Tahkoubit Khaled

**Abstract** MC-CDMA is the most promising technique for high bit rate and capacity transmission in wireless communication. One of the challenging issues of MC-CDMA system is the very high PAPR due to the large number of sub-carriers which reduces the system efficiency. In our work a new (SLM-PTS) method is suggested with one IFFT block for PAPR reduction in MC-CDMA downlink transmission. The new method has showed a significant improvement in PAPR reduction performance and system complexity. SLM-PTS is compared to PTS and SLM at the term of PAPR reduction, as well as it is compared to the original system at the term of bit-error-rate (BER), firstly, without and then using the linear amplifier (SSPA).

**Index Terms** IFFT, MC-CDMA, PAPR, PTS, SLM, SSPA.

## I. INTRODUCTION

It is well known that high bit rate transmission is required for high quality broadband wireless communication. The 21st century systems (3rd generation and beyond) have to support a large range of multimedia services such as speech, images and data with different and variable bit rates up to 2 Mbits/s. Future radio communication systems will have to accommodate high data rate while allowing a great mobility to the users. In order to achieve this goal, new signal processing techniques must be investigated. In this paper, one of the techniques under current significant research, namely the MC-CDMA (Multi-Carrier Code Division Multiple Access) technique, is suggested.

The code-division multiple access system has higher frequency efficiency than conventional time division multiple access (TDMA) or frequency division multiple access (FDMA) systems. However, the capacity is limited by the inter-chip interference (ICI) and multiple-access interference (MAI). Besides, multi-carrier (MC) transmission technique has many advantages such as high bandwidth efficiency, excellent frequency diversity, and high speed parallel transmission. When subcarrier number is chosen appropriately, there is only flat fading that has no ICI in each sub-channel. Recently, considerable interests are focused on the combined scheme of OFDM and CDMA [1].

MC-CDMA is a very attractive technique for a high speed data transmission over the multipath fading channels. High Peak to Average Power Ratio (PAPR) of the transmitted

signal is a serious problem in multicarrier systems (MC), such as Orthogonal Frequency Division Multiplexing (OFDM), or in Multi-Carrier Code Division Multiple Access (MC-CDMA) systems, due to large number of subcarriers. This effect is possible to reduce with some PAPR reduction techniques. High Power Amplifier (HPA) have big influence on the behavior of the system, which results in a large degradation of performance, i.e. increase of both the bit error rate (BER) and the out-band radiation (spectral spreading). Since decades, many solutions have been proposed to solve this problem. Some of them compensate for non-linearities at the transmitter side and some of them carry out the processing at the receiver side. It is necessary first to distinguish between processing on the amplification function and processing on the signal itself.

To reduce the PAPR, various techniques have been proposed in literature including the clipping and filtering technique [2][3], the Partial Transmit Sequences (PTS) [4] [5], the Selective Mapping (SLM) method [6], and Tone Reservation (TR) [7], etc...

Our work is organized as follows. In Section two, general concepts of a MC-CDMA system are explained; definition and mathematical expression of the PAPR are also given. In Section three a new (SLM-PTS) method for PAPR reducing purposes is proposed. The simulation results are described in section four. The last Section provides some conclusions.

## II. MC-CDMA SYSTEMS

In an MC-CDMA system [8, 9] a block of  $M$  information symbols from each active user are spread in the frequency domain into  $N = L.M$  subcarriers, where  $L$  represents the spreading factor. This is accomplished by multiplying every symbol of the block for user  $k$ , where  $k = 1, 2, \dots, K$ , by a spreading code  $C_j$ .  $C_j$  is selected from a set of  $L$  orthogonal sequences, thus, allowing a maximum of  $L$  simultaneous users to share the same radio channels. The spreading codes are the usual Walsh-Hadamard (WH) sequences, which are the columns of the Hadamard matrix of order  $L$ . If  $L$  is a power of 2, the Hadamard matrix is constructed recursively as

$$H_L = \begin{bmatrix} H_{L/2} & H_{L/2} \\ H_{L/2} & -H_{L/2} \end{bmatrix} \quad (1)$$

where the symbol «\*» denotes de Kronecker tensor product.

In the downlink transmitter, each spread symbol of every active user is added to the spread symbols of the remaining

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active users, and the resulting sums are interleaved to form a set of  $0 \leq l \leq L-1$  complex amplitudes as follows:

$$s_l = \sum_{k=1}^{K} a_k e^{j\theta_k} c_{l, k} \quad (2)$$

where  $K$  is the total number of active users and  $a_k$  is the peak power of the SSPA.  $c_{l, k}$  are the data symbols in the block for the  $k$  active user.

After Inverse Fast Fourier Transform (IFFT) operation, the time domain signal  $x(n)$  is given by

$$x(n) = \sum_{l=0}^{L-1} s_l e^{j2\pi f_c n T} \quad (3)$$

where  $J$  is the oversampling factor integer.

A. Peak to Average Power Ratio (PAPR)

The PAPR of a complex signal  $x(n)$  can be defined as the ratio of the peak envelope power to the average envelope power:

$$PAPR = \frac{\max_n |x(n)|^2}{\frac{1}{N} \sum_{n=0}^{N-1} |x(n)|^2} \quad (4)$$

where  $\mathbb{E}\{\cdot\}$  represents the expectation operation.

The Complementary Cumulative Distribution Functions CCDF formula that approximates the PAPR of a multicarrier signal with Nyquist sampling rate is derived from the central limit theorem [10] and is given by:

$$P(PAPR > \gamma) \approx \frac{1}{\gamma} e^{-\gamma} \quad (5)$$

where  $\gamma$  indicates the threshold value.

B. Solid State Power Amplifier (SSPA)

The SSPA [11] demonstrates non-linear characteristics, as it causes distortion of the signals, particularly the high PAPR values. Therefore, the BER performance of the system is decreased. The input and output signals of the SSPA are defined as:

$$y(n) = \sum_{k=1}^K A_k |x(n)|^{2\alpha} e^{j\phi_k} \quad (6)$$

$$y(n) = \sum_{k=1}^K A_k |x(n)|^{2\alpha} e^{j\phi_k} \quad (7)$$

Respectively,  $x(n)$  is the input signal amplitude,  $\phi_k$  is the input signal phase,  $A_k$  is the output signal amplitude and  $\phi_k$  is the output phase response. Amplitude/amplitude (AM/AM) and amplitude/phase (AM/PM) characteristics of the SSPA are defined as:

$$\hat{A}_k = \frac{A_k}{A_0} \quad (8)$$

where  $A_0$  is the output saturation amplitude and  $\alpha$  is the smoothness control coefficient. The operating point of the SSPA is determined by the Input Back-Off (IBO) parameter and is expressed as:

$$P_{out} = \sum_{k=1}^K P_{in, k} \quad (9)$$

where  $P_{in, k}$  is the mean power of the input signal and  $P_{out}$  is the peak power of the SSPA.

Fig. 1 represents the MC-CDMA downlink transmitter.

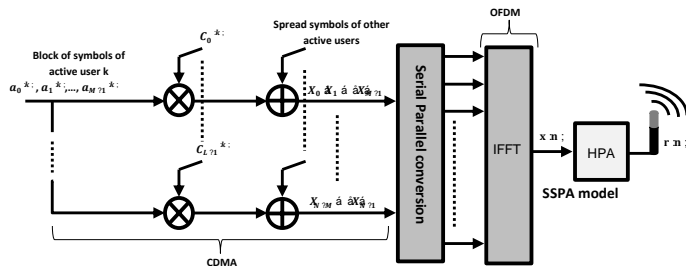


Fig. 1. MC-CDMA downlink transmitter.

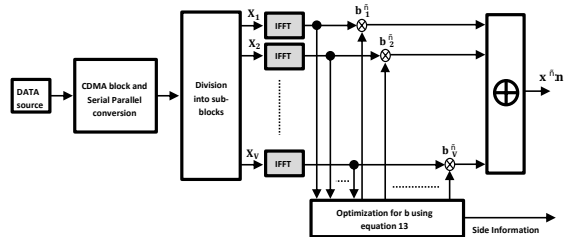


Fig. 2. Block diagram of the PTS techniques.

C. The Partial Transmit Sequences (PTS) technique

In the PTS technique [12], the input data blocks are partitioned into disjoint subblocks  $x_k = [x_{k,0}, x_{k,1}, \dots, x_{k,L-1}]^T$ ,  $k = 1, \dots, V$ , such that:

$$\sum_{k=1}^V x_k = 0 \quad (10)$$

Complex phase factors are  $b_k = [b_{k,0}, b_{k,1}, \dots, b_{k,L-1}]^T$ ,  $k = 1, \dots, V$ . The set of the phase factors shall be written as a vector  $\mathbf{b} = [b_{1,0}, b_{1,1}, \dots, b_{V,L-1}]^T$ . The time-domain signal after combining is given by:

$$x'(n) = \sum_{k=1}^V \sum_{l=0}^{L-1} x_{k,l} e^{j2\pi f_c n T} b_{k,l} \quad (11)$$

After Inverse Fast Fourier Transform (IFFT) operation, the time domain signal  $x'(n)$  is given by

$$x'(n) = \sum_{k=1}^V \sum_{l=0}^{L-1} x_{k,l} e^{j2\pi f_c n T} b_{k,l} \quad (12)$$

The objective is to find the phase factors with the aim of minimizing PAPR. This is related to the minimization of:

$$PAPR = \frac{\max_n |x'(n)|^2}{\frac{1}{N} \sum_{n=0}^{N-1} |x'(n)|^2} \quad (13)$$

Fig. 2 shows the block diagram of PTS technique.

In our work only one subblock of IFFT is retained to simplify this technique; the subblocks of data should be



IV. SIMULATION RESULTS

It has been used  $s_{qp}$  users,  $L$  tw sub-carriers, a Walsh Hadamard spreading code of length  $L$  and a 16-QAM modulation, for the MC-CDMA system. The oversampling factor of the system is  $L$ . The number of sub-blocks  $L_s$  and  $L_t$  are chosen for the SLM optimization whereas the different values of the parameters  $U$  and  $8 : 8 \acute{a} 9 L : v \acute{a} v ; \acute{a} : z \acute{a} t ; \acute{a} : v \acute{a} r e ;$  chosen in the PTS optimization. In the new SLM-PTS optimization,  $: 7 \acute{a} 8 \acute{a} 9 ; x \acute{v} \acute{a} v \acute{s} \acute{x} \acute{a} : v \acute{a} x \acute{y} \acute{a} : v \acute{s} \acute{x} \acute{a} v \acute{a}$  has been chosen. The SSPA is used with  $L_s t \acute{a}$  and  $u @ \$$  and smoothness factor  $L$ . The communication channel is Rayleigh fading. First the SLM, PTS and SLM-PTS methods are compared in terms of PAPR reduction performances in the MC-CDMA system. Moreover, the BER performance of the MC-CDMA system using SLM-PTS is shown when the SSPA and the linear amplifier are used.

A. PAPR Reduction

Fig. 7 illustrates the complementary cumulative distribution functions (CCDF) of the PAPR for original signals and other signals obtained by the SLM scheme. One can notice from the simulation results, that the SLM scheme for  $7 L \times$  provides better PAPR reduction comparing to the SLM scheme with  $L16, 8$  and  $4$ . Given  $7 L \times$  provides a PAPR reduction of  $2.7\text{dB}$  at  $10^{-5}$ , while, taking  $7 L$  provides PAPR reduction of only  $1 \text{ dB}$  at  $10^{-5}$ . It is known that the SLM scheme requires  $\acute{a} \acute{a} \acute{a} \acute{a}$  numbers of complex multiplications  $\bullet_{k_s j}$ ; and  $\acute{a} \acute{a} \acute{a} \acute{a}$  numbers of complex additions  $\bullet_{-bb}$ ; thus, for  $L v \acute{a} z \acute{a}$  the SLM scheme the calculating complexity is  $\bullet_{k_s j} L v u r r \acute{z} x r s \acute{s} y t r u t$  and  $\bullet_{-bb} L z s \{ t \acute{s} x u z \acute{v} r t y x z$  respectively.

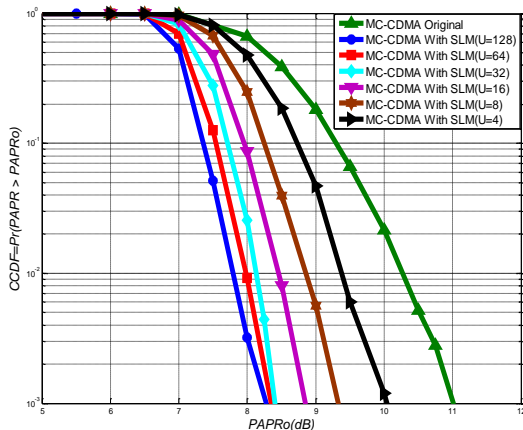


Fig. 7. PAPR reduction performance for SLM regarding different values of the parameter U.

Fig. 8 shows the Complementary Cumulative Distribution Functions (CCDF) of the PAPR for original signals and other signals obtained by the PTS scheme. Increased values of  $: 8 \acute{a} 9$  offers better PAPR reduction. For example, given  $: 8 \acute{a} 9 ; L : t r \acute{a} r t s$  scheme provides only  $\acute{a} y @ \$$  the PAPR at  $10^{-5}$ , however, this value goes up to  $u @ \$$  with  $: 8 \acute{a} 9 ; L : z$ . Therefore, PTS explores all the phase vectors to find the lowest value of the PAPR requiring  $v \acute{s} \acute{a} L x v$  and  $t \acute{z} \acute{s} L s t z$  check in respectively.

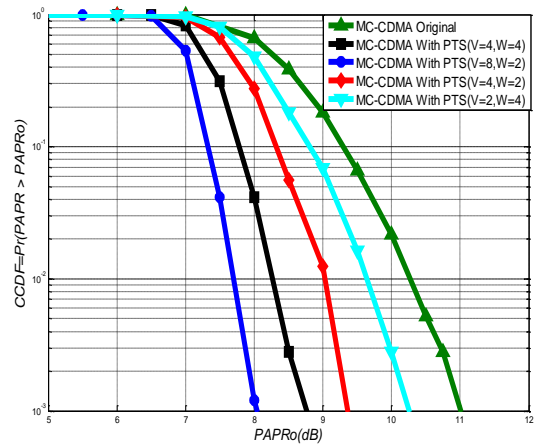


Fig. 8. PAPR reduction performances for PTS regarding different values of V and U parameters.

Fig. 9 shows the Complementary Cumulative Distribution Functions (CCDF) of the PAPR for original signals and other signals obtained by the SLM-PTS scheme. The SLM-PTS scheme for  $: 7 \acute{a} 8 \acute{a} 9 ; x \acute{v} \acute{a} v \acute{s} \acute{x} \acute{a} : v \acute{a} x \acute{y} \acute{a} : v \acute{s} \acute{x} \acute{a} v \acute{a}$  provides better PAPR reduction of  $t \acute{z} \acute{s} @ \$ \% \& ( s \acute{r} \acute{z} \acute{z} \acute{z}$ , comparing tot  $\acute{a} w @ \$$  obtained with  $: 7 \acute{a} 8 \acute{a} 9 ; x \acute{v} \acute{a} v \acute{a} t ;$

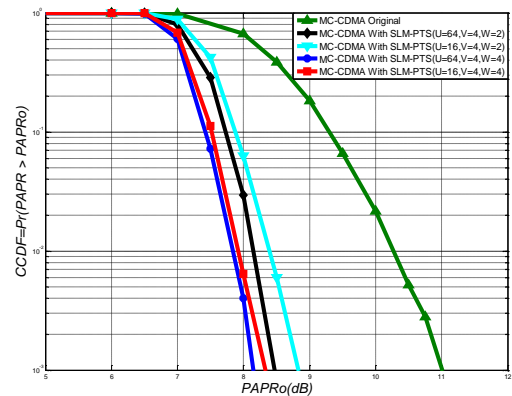


Fig. 9. PAPR reduction performance for SLM-PTS regarding different values of U, V and W parameters.

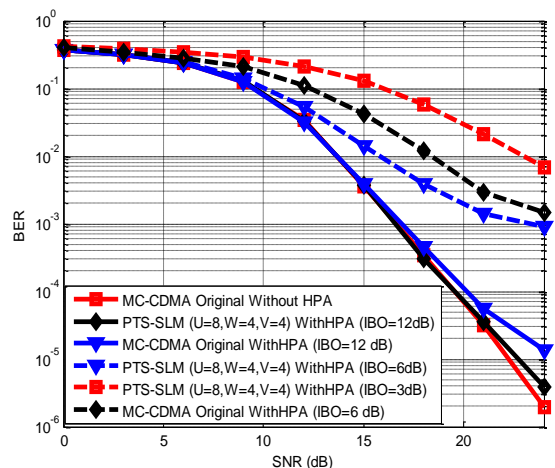


Fig. 10. BER performance with 16-QAM and different IBO over Rayleigh fading channel.

B. BER Performance

Figure. 10 shows the BER performance of the SLM-PTS scheme for 16-QAM and  $7 \acute{a} 8 \acute{a} 9 ; L : t r \acute{a} r t s$  back off  $+ \$ 1 L s t \acute{a} x @ \$$  in Rayleigh fading channels. The represented curves of Fig.10 are obtained for the cases of the

original signal transmitted without SSPA (MC-CDMA original without HPA), the SLM-PTS scheme with SSPA and the original signal transmitted with SSPA (MC-CDMA original with HPA) respectively. According to obtained results the IBO remains very important for the BER performance of the system. The new method (SLM-PTS) which is presented in this work, offers better performance of the MC-CDMA original with HPA. For example, the PAPR reduction is 1.7 dB at 5.04 dB, whereas the PAPR reduction is 1.7 dB at 5.04 dB + 1.7 dB.

## V. CONCLUSION

In the present work, a new method has been presented to reduce the PAPR in MC-CDMA systems. Moreover, calculating complexity of the new system is improved. This technique combines the PTS and SLM techniques and does not need IFFT subblocks. Simulation results were achieved by comparing the studied method to the original system in term of BER and CCDF. Obtained results showed that the proposed method is less complex and exhibits significant performance in term BER and CCDF.

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