

beam-to-column connections with steel dowels for global analyses of precast buildings. The analytical model was developed on the basis of the expressions and the results reported by [2]-[5]. The model allows to define the behaviour of beam-to-column connections by means of bilinear force-displacement curve for monotonic loading and trilinear force-displacement curve for cyclic loading. The model was calibrated and verified on the basis of the experimental results and considers the effects of different parameters (dowel diameter, geometry of connection, material properties).

Fig. 2 shows the analytical bilinear curve for the two monotonic tests, push and pull, in case of connection with $2\Phi 25$ dowels. The theoretical curve approximates well the experimental results in the elastic and plastic ranges. The maximum force in the pull-direction was significantly smaller than in the push-direction due to the failure of the concrete cover in the front side of the beam.

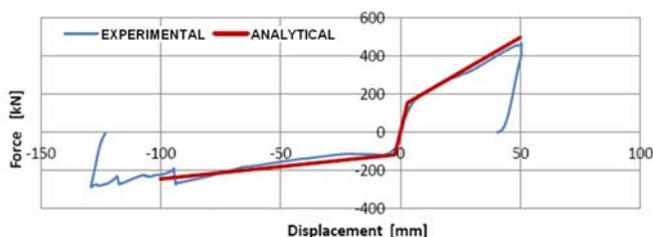


Fig. 2. Force - displacement relationship: Comparison of analytical and experimental results for monotonic test.

Fig. 3 shows the analytical trilinear curve compared to the experimental results of the cyclic tests. A good agreement can be observed in terms of stiffness, maximum load and softening branch up to collapse. As expected, the response was not symmetric in the push- and the pull-direction, because the resistance in the pull-direction was reduced due to the small cover of the dowels.

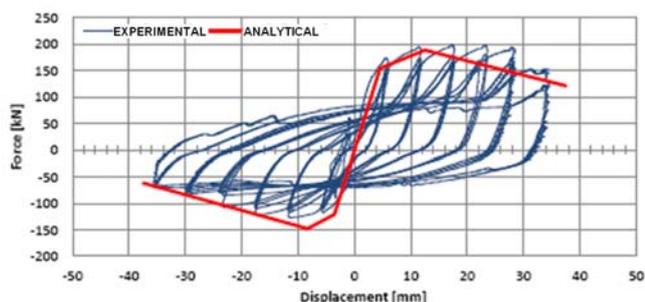


Fig. 3. Force - displacement relationship: Comparison of analytical and experimental results for cyclic test.

The models were extended and validated considering other types of specimens with different characteristics (number, diameter and cover of the dowels). Good correlation with experimental results was obtained, confirming the effectiveness of the model.

III. CASE STUDY BUILDING

Some reference existing buildings, representative of

typical structural solutions for precast industrial buildings built in Italy, were modelled and analyzed under earthquake loading. This study presents and discusses the relevant results of numerical analyses performed on a precast industrial building, designed according to Italian Standard (2008) for a peak ground acceleration $a_g=0.16g$ and soil class B. Concrete C45/55 and steel B450C were used for the design. The building presents a regular structural scheme with a rectangular plan: the longitudinal side is equal to 33.1m and the transverse one is equal to 39.5m. The square columns (60cm x 60cm), whose height is equal to 6.7m, are connected by prestressed RC beams, parallel to the longitudinal direction, with I-shaped constant section. The length of the prestressed beams is 8.1m. Elements with length equal to 19.5m and V-shaped constant section are located on the main beams and represent the roof of the building. The connections between the main beams and the columns consist of $2\Phi 25$ steel dowels.

The case study building was numerically modelled using both the general purpose finite element code Straus and the nonlinear dynamic analysis software Ruaumoko, widespread used in academic research. Two different modelling approaches were employed and two complementary models were developed by using the two codes. A schematic view of the numerical model developed for the case study building with notation of some reference columns is presented in Fig. 4. Two variants of the model of the building were developed, hereafter named as model M1 and model M2. The first model M1 presented simple pinned beam-to-column connections. In the second model the beam-to-column connections were modelled using spring elements. The force-displacement relationships adopted to model the behaviour of the beam-to-column connections were derived from the analytical models calibrated and validated with the results of the experimental tests. The Takeda hysteresis rule, implemented in the computer codes Straus and Ruaumoko, was adopted to reproduce the cyclic behaviour of the beam-to-column connections.

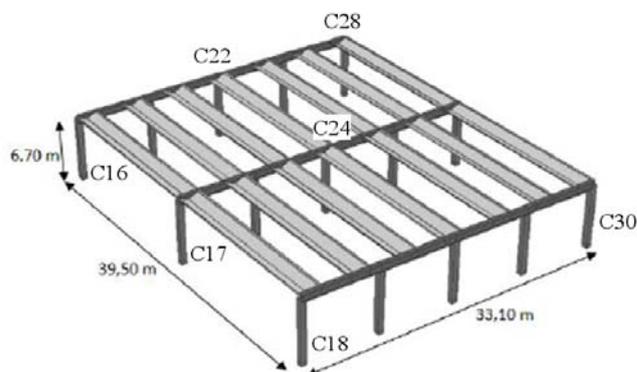


Fig. 4. Numerical model of the building and notation of columns.

IV. NONLINEAR DYNAMIC ANALYSES

Bidirectional nonlinear dynamic analyses with increasing intensity levels were performed on the two models M1 and M2. Artificial ground motion records with 20s duration were generated by using the code SIMQKE in order to match the

Eurocode 8 response spectrum (type 1, subsoil class B).

Fig. 5 shows the maximum top displacement in the longitudinal direction (direction y) for the two models at different seismic intensity levels ranging from 0.1g to 0.4g. In case of low seismic intensity level larger displacements are observed for the model M2; on the contrary, a reduction of 11% is registered for the model M2 at 0.4g seismic intensity level.

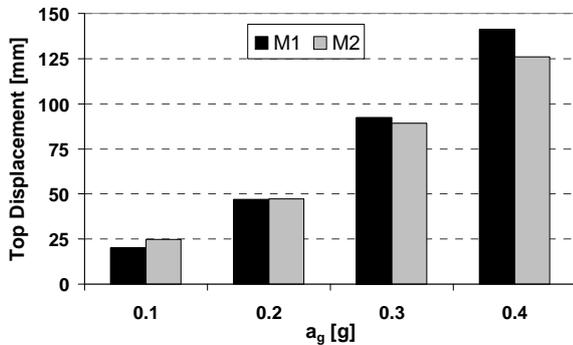


Fig. 5. Maximum top displacement for the models M1 and M2 at different seismic intensity levels.

The maximum axial forces acting on some reference columns of the two models at 0.4g seismic intensity level are presented in Fig. 6. The maximum value of the axial force is registered for the internal column C24. A maximum reduction equal to 13% is computed for the external columns C16 and C28 of the model M2.

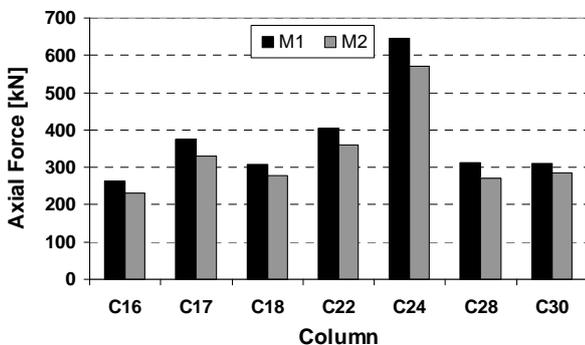


Fig. 6. Maximum axial force for the columns of the models M1 and M2 at 0.4g seismic intensity level.

The Demand-to-Capacity Ratio (DCR), i.e. the ratio between the chord rotation demand and chord rotation capacity, was used to evaluate the damage level of columns. The maximum rotation demand was obtained by numerical analyses and the rotation capacity was computed according to Eurocode 8 Part 3. Fig. 7 shows the maximum DCR values for some reference columns of the two models at 0.4g seismic intensity level. High DCR values close to 0.8 can be observed for some columns of the model M1. Significant decreases of the DCR values are registered for all the columns of the model M2, with maximum reductions of 30% for the external columns C18 and C30. Numerical results suggest that the

building under study exhibits high levels of ductility, dissipating significant amount of energy through inelastic behaviour. The maximum DCR values confirm that the building is able to withstand stronger seismic excitations, beyond the design earthquake.

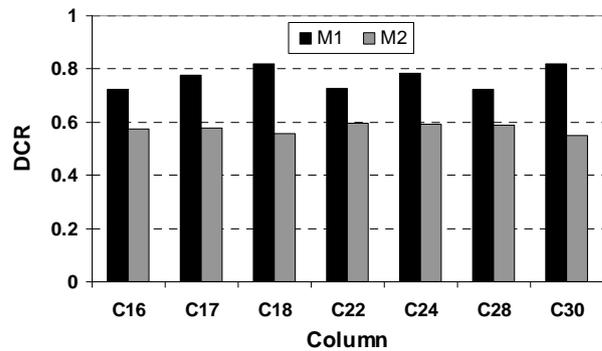


Fig. 7. Maximum DCR values for the columns of the models M1 and M2 at 0.4g seismic intensity level.

Fig. 8 shows the energy dissipated by the models M1 and M2 (columns and beam-to-column connections) for different seismic intensity levels. The total energy dissipated by the structure is larger for the model M2, but the plastic demand on columns is higher for the model M1. A considerable reduction (equal to 20%) of the energy dissipated by the columns of the model M2 is observed at 0.4g seismic intensity level due to the energy dissipation contribution of the beam-to-column connections. The difference of plastic demands on the columns of the two models increases as the seismic intensity level increases.

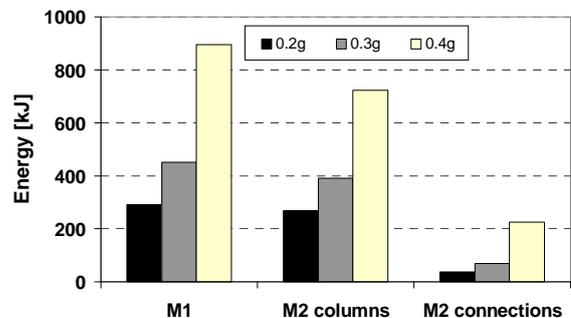


Fig. 8. Energy dissipated by the models M1 and M2 (columns and connections) at different seismic intensity levels.

The behaviour of the beam-to-column connections of the model M2 was examined at 0.4g seismic intensity level. Fig. 9 reports the maximum displacement and force values achieved in some relevant connections of the model during seismic excitation, for push and pull directions. Numerical results show that the contribution of the connections is mainly influenced by their position in the model. The external connections significantly entered into the plastic range, while a large part of the internal connections remained in the elastic range.

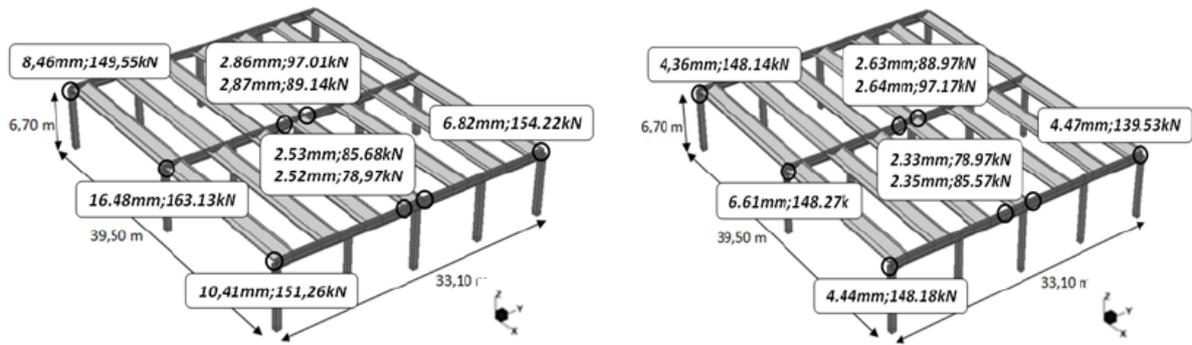


Fig. 9. Maximum displacement and force values for some springs of the model M2 at 0.4g seismic intensity level: push (left) and pull (right) direction.

It can be noted that all the connections didn't achieve failure, even for 0.4g seismic intensity level.

In the model M2 the formation of the first plastic hinge at the column base was delayed compared to the model M1. During time-history analysis with artificial accelerogram with 20 seconds duration, the first plastic hinge occurred at the column base after 3.9 seconds in the model M1 and after 4.2 seconds in the model M2. Moreover, after 5 seconds all the columns of the model M1 presented plastic hinges at the base, while in the model M2 some columns were still in the elastic range.

V. CONCLUSION

The main results of a numerical study on the seismic response of a precast industrial building subjected to earthquake excitation were presented. Analytical models developed on the basis of experimental tests were used to simulate the behaviour of beam-to-column connections with steel dowels for nonlinear dynamic analyses of precast buildings. The models were extended to consider the effects of different parameters and correlated well with experimental results. The effects of numerical modelling of beam-to-column connections on the seismic response of a precast industrial building were investigated and comparisons with the model with simple pinned beam-to-column connections were performed. The use of refined models of beam-to-column connections significantly decreased plastic strain demands at the column base and a reduction of the damage level was observed for the columns of the building compared to the case of model with simple pinned beam-to-column connections. The formation of the

first plastic hinge at the column base was delayed. The building exhibited high levels of ductility, dissipating significant amount of energy through inelastic behaviour. The DCR values showed that the building was able to withstand stronger seismic excitations, beyond the design earthquake. The energy dissipation contribution of the connections was mainly influenced by their position in the model. The external connections presented significant inelastic deformations, while a large part of internal connections remained in the elastic range. It can be noted that all the connections didn't achieve failure, even for 0.4g seismic intensity level.

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