

# Using Fuzzy Logic Self-Tuning PI Gain Controller Z-Source Inverter in Hybrid Electric Vehicles

An Wen Shen, Cong-Thanh Pham, Phan Quoc Dzung, Nguyen Bao Anh, and Le Hoang Viet

**Abstract**—This paper presents a new algorithm to control the peak dc-link voltage (PDV) across the inverter bridge in Z-Source inverters (ZSI) by applying self-tuning fuzzy PI controller (SFP) with robust structure and non-linear characteristic. In particular, this so-called SFP based control algorithm is applied to closed loop speed control system of induction motor, which relies on direct torque control combined with modified space vector modulation (DTC-MSVM) control strategy. More importantly, the combination of SFP based control algorithm and DTC-MSVM with many exceptional features such as: fast torque response, low steady state torque ripple, and high accurate is the best candidate for controlling the PDV in hybrid electric vehicles (HEV) applications. In this way, the PDV is more adaptive to the sudden change of dc input voltage (DIV). The transient response of PDV is thus improved with low disturbance for output voltage stabilization in the inverter bridge. As a result, we achieve higher robustness and performance of speed motor control system. Our new SFP based control algorithm is verified in both simulation and experimental implementation using MATLAB and dSPACE DS1103, respectively.

**Index Terms**—Buck-boost; PWM; DTC-SVM; voltage source inverters (VSIs), induction motor speed control; z-source inverter; hybrid electric vehicles.

## I. INTRODUCTION

In a conventional voltage source inverter, the two switches of any phase leg cannot be gated at the same time because this may cause a short circuit situation and thus destroy the inverter. In addition, the maximum output voltage cannot exceed the dc bus voltage. These limitations in such conventional voltage source inverter can be overcome by using ZSI [1]. Actually, the ZSI is a power electronic converter with many advantages such as buck-boost characteristics, lower cost, and especially higher efficiency compared to traditional dc-dc converter [2], [3]. As a more sophisticated design of ZSI, high-performance ZSI (HP-ZSI) copes with dc-link voltage drops for wide range of load with even using small inductor while guaranteeing a simple design. Thus, HP-ZSI is more suitable for HEV applications [4], [5].

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AnWen Shen is with the Dept of Control Science and Engineering, Huazhong University of Science and Technology, Wuhan, China.

Cong-Thanh Pham is with the Dept of Control Science and Engineering, Huazhong University of Science and Technology, Wuhan, China; HCMC University of Technology, Ho Chi Minh City, Vietnam; Electrical and Electronics Engineering Faculty, HCMC University of Transport, Ho Chi Minh City, Vietnam.

Phan Quoc Dzung is with the HCMC University of Technology, Ho Chi Minh City, Vietnam (email: phamcongthanh09@yahoo.com).

Nguyen Bao Anh and Le Hoang Viet are with the HCMC University of Technology, Ho Chi Minh City, Vietnam.

In control systems of the HEV, the control requirements are very high and stringent; they are fast torque response, low steady state torque ripple, high accuracy, wide speed range, and high torque at low speed. It is really challenging to meet all of these requirements by using traditional control methods of induction motor (IM) such as: voltage/hezt, field oriented control and traditional direct torque control, but DTC-SVM control method can succeed [6], [7].

In HP-ZSI, the dc link voltage is in square waveform, it is zero when the inverter bridge is in the shoot-through zero state, but is peak value when the inverter bridge is in the non-shoot-through state [1]. Consequently, the dc link voltage cannot be controlled directly. Alternatively, there have been many studies proposed to control the average value of dc link voltage by controlling the capacitor voltage. However, the capacitor voltage ( $V_c$ ) is somewhat equivalent to the PDV of inverter, which the relationship between the PDV ( $\hat{V}_i$ ) and the capacitor voltage are the non-linear. Additionally, when ZSI parameters (resistor of capacitor, capacitor, resistor of inductor, inductor, shoot through duty  $d_o$ ) are variations, non-minimum phase phenomenon of ( $\hat{V}_i/d_o$ ) transfer function is more serious than that of the control to ( $V_c/d_o$ ) transfer function [8]. Therefore, controlling the value of dc link voltage by controlling the PDV is most suitable for ZSI.

In this paper, applying SFP to control the PDV is promise for non-minimum-phase or non-linear characteristic of ZSI. In particular, SFP means that the two parameters  $K_p$ ,  $K_i$  of conventional PI controller are tuned by using fuzzy inference tuner to improve quality control of non-linear systems such as: without error steady state, less overshoot, decrease rise time and faster settling time. SFP of ZSI is set up to closed loop speed control system of induction motor, which relies on DTC-MSVM control strategy. More importantly, the combination of SFP and DTC-MSVM with many exceptional features such as: fast torque response, low steady state torque ripple, and high accurate is the best candidate for controlling the PDV in HEV applications. In this way, the PDV is more adaptive to the sudden change of DIV. The transient response of PDV is thus improved with low disturbance for output voltage stabilization in the inverter bridge. As a result, we achieve higher robustness and performance of speed motor control system. Our new SFP based control algorithm is verified in both simulation and experimental implementation using MATLAB and dSPACE DS1103, respectively.

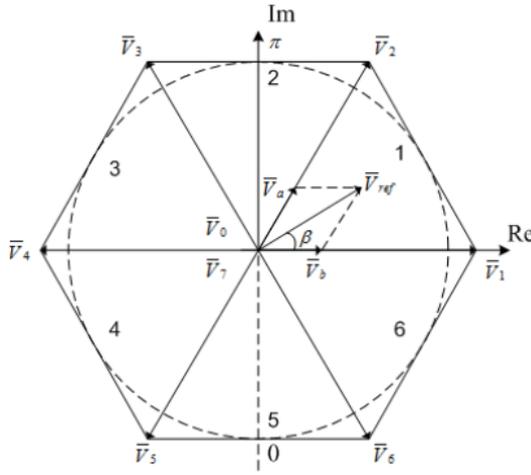


Fig. 1. Voltage vector through conventional SVM of VSI.

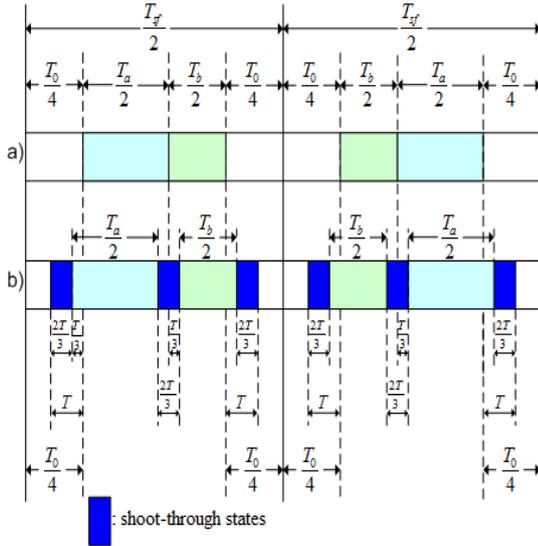


Fig. 2. Modified space vector PWM (MSVM). a) Switching

## II. ANALYSIS CONTROL METHODS

### A. Dynamic Model of Induction Motor (IM), DTC-SVM

#### 1) Nomenclature

Three-phase IM 1Hp model in stationary frame equation base on dynamic model (Kron Equation) [11] are given as:

- $v_{dqs} = v_{ds}; v_{qs} =$  d-axis; q-axis stator voltages;
- $i_{dqs} = i_{ds}; i_{qs} =$  d-axis ; q-axis stator currents;
- $\Phi_{dqs} = \Phi_{ds}; \Phi_{qs} =$  d-axis; q-axis rotor flux linkages;
- $T_e; T_l =$  The electromagnetic torque; load torque;

#### 2) Dynamic model of IM

The corresponding stationary frame equations [11] can be derived easily as follows:

Stator Voltage:

$$v_{dqs} = R_s i_{dqs} + \frac{d\Phi_{dqs}}{dt} \quad (1)$$

Rotor Voltage:

$$0 = R_r i_{dqr} + \frac{d\Phi_{dqr}}{dt} \pm \omega_r \Phi_{dqr} \quad (2)$$

Stator Flux:

$$\Phi_{dqs} = L_{ls} i_{dqs} + L_m (i_{dqs} + i_{dqr}) \quad (3)$$

Rotor Flux:

$$\Phi_{dqr} = L_{lr} i_{dqr} + L_m (i_{dqs} + i_{dqr}) \quad (4)$$

Mechanical:

$$T_e = \frac{3}{2} \frac{p}{2} (\Phi_{ds} i_{qs} - \Phi_{qs} i_{ds}) \quad (5)$$

$$T_e - T_l = J_m \frac{2}{p} \frac{d\omega_r}{dt} + B_m \omega_r \quad (6)$$

### B. Direct Torque Control-Modified Space vector Modulation (DTC-MSVM)

#### 1) MSVM

The space vector pulse width modulation (SVM) method have widely used at regulated PWM inverter due to a higher modulation index and lower current harmonics in [12]. Base on principles of ZSI [13], the shoot-through states (STS) should be inserted period intervals of SVM are called the modified space vector modulation (MSVM) to boost-buck the dc-link voltage of the ZSI, to reduce the common (RCM) voltage, not require dead-time protection short circuit at two switches any of the same phase leg and to achieve alike optimal harmonic performance by given [1] and are expressed at Fig. 2 b).

where  $V_0, V_7$  are two zero vectors and STS is the third zero vector in ZSI, where  $V_1$  to  $V_6$  are the six active vectors in Fig. 1. When  $V_{ref}$  rotate around section (1-6) of hexagon while (a, b) are changed: (a, b) = (1, 2); (2, 3); (3, 4); (4, 5); (5, 6) in every sector, respectively. In one sampling interval,  $V_a$  and  $V_b$  are applied at times  $T_a$  and  $T_b$ , respectively, and the zero vector is applied at time  $T_{sf} = (T_a + T_b) + T'_0 + T_{sr}$  where  $T'_0 = T_0 - T_{sr}$ . Consequently, from (7), the reference voltage vector  $V_{ref}$  can be given by

$$\vec{V}_{ref} = \vec{V}_a T_a + \vec{V}_b T_b \quad (7)$$

$$T_a = \sqrt{3} \cdot \frac{V_{ref}}{V_i} \cdot T_{sf} \cdot \sin\left(\frac{\pi}{3} - \beta\right) \quad (8)$$

$$T_b = \sqrt{3} \cdot \frac{V_{ref}}{V_i} \cdot T_{sf} \cdot \sin(\beta) \quad (9)$$

where  $\beta$  is the angle between the reference voltage vector  $V_{ref}$  and voltage vector  $V_1$ ,  $\hat{V}_i$  is the PDV.

The MSVM Fig. 2b). where  $T_{sr}$  is shoot-through time. From Fig. 2. the STS are evenly assigned to each phase with  $2T/3$  within zero voltage period  $T_0/4$  and  $T/3$  within active voltage period  $T_0/2$  and  $T/3$  within active voltage period  $T_0/2$ , where  $T_a$  and  $T_b$  are unchanged. So the STS does not affect the SVM control method of the inverter, and it is limited to the zero state time  $T_0$ . Where  $T$  are determined by (10).

$$T_{sr} = 6.2 \cdot \frac{T}{3} = 4T \rightarrow T = \frac{T_{sr}}{4} \quad (10)$$

And from [14] we have

$$o < d_0 = \frac{T_{sr}}{T_{sf}} < \frac{1}{2} \rightarrow o < T_{sr} < \frac{T_{sf}}{2} \quad (11)$$

where  $d_o$  is shoot through duty. From (10) and (11) we have:

$$0 < T < \frac{T_{sf}}{8} \quad (12)$$

Therefore, controlling the dc-peak voltage across the inverter bridge have to found on limited of time T.

### 2) DTC-MSVM

The DTC-MSVM are combined from DTC and MSVM Fig. 2. The DTC-MSVM there are features the same with DTC-SVM such as: fast torque response, low steady-state torque ripple, low current distortion, high-performance dynamic characteristics and accuracy. Especially the aim of this method to control the PDV ( $\hat{V}_i$ ) by regulate STS while DIV decrease or increase that is not affect speed control and torque motor [5], [7]. Therefore, the DTC-MSVM is the best candidate for HEV applications Fig. 3.

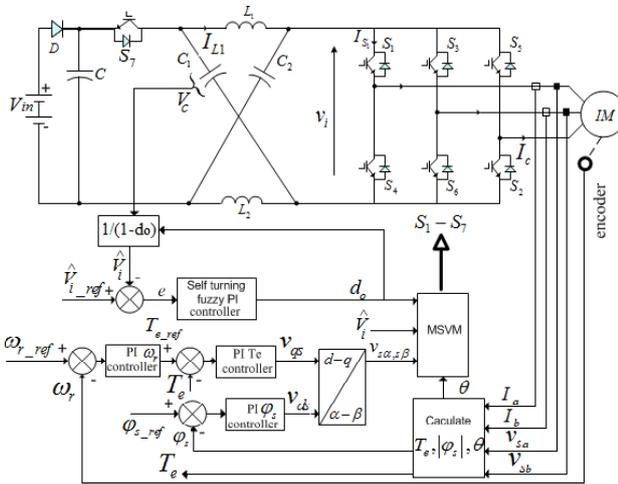


Fig. 3. DTC-MSVM block diagram.

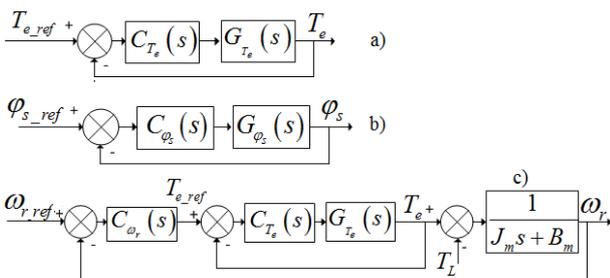


Fig. 4. Block diagram electromagnetic torque a) stator flux controller b) and speed controller controller c).

### C. A new Algorithm Control the PDV across the Inverter Bridge Due to SFP, Stator flux Controller, Electromagnetic Torque Controller, Speed Controller

#### 1) Electromagnetic torque controller

The electromagnetic torque open loop dynamics is presented by the writing of the closed loop transfer function is divided between the electromagnetic torque and the q-axis stator voltage [15]. The open loop transfer function  $G_{Te}(s)$  in s-plane is expressed by:

$$G_{Te}(s) = \frac{T_e(s)}{V_{qs}(s)} = \frac{s + A_{Te}}{s^2 + B_{Te}s + C_{Te}} \quad (13)$$

where:

$$A_{Te} = \frac{K_t L_r}{\sigma}; B_{Te} = \frac{R_s L_r + R_r L_s}{\sigma}; C_{Te} = \frac{3p^2 K_t L_r |\phi_{s-ref}|^2}{2J_m \sigma}$$

$\sigma = L_r L_s - L_m^2$ . All of these parameters are given in TABLE I.

Electromagnetic torque controller parameters  $C_{Te}(s)$  are calculated in sisotool of Matlab, base on PI controller Fig. 4 a), Fig. 3.

#### 2) Stator flux controller

Especially, the dynamic flux in open loop is presented by the writing of the closed loop transfer function between stator flux and d-axis stator voltage that based on the motor model (1) to (4) and from [15] the open-loop flux transfer function  $G_{\phi}(s)$  in s-plane is written by:

$$G_{\phi}(s) = \frac{\Phi_{ds}(s)}{V_{ds}(s)} = \frac{s + A_{\phi}}{s^2 + B_{\phi}s + C_{\phi}} \quad (14)$$

where:  $A_{\phi} = \frac{L_r L_s}{\sigma}; B_{Te} = B_{\phi}; C_{\phi} = \frac{R_r R_s}{\sigma}$ . All of these parameters are also given in TABLE I. Flux controller parameters  $C_{\phi}(s)$  are also calculated in sisotool of Matlab, base on PI controller Fig. 4b), Fig. 3.

#### 3) Speed controller

Because of the variation of the load torque, speed controller motor is designed based on Fig. 4c), [5] so that it obtain the required response during load changes is given by:

$$K_{p\omega_r} = 2J_m \xi \omega_n - B_m \quad (15)$$

$$K_{i\omega_r} = J_m \xi \omega_n^2 (2\xi^2 - 1) \quad (16)$$

where:  $\omega_n$  and  $\xi$  are the dynamics response and desired damping, respectively.

#### 4) A new algorithm control the PDV across the inverter bridge due to SFP

The PID controller is the most popular controller and widely used to improve the performance of systems control in industry. Additionally, for some small inertia of systems, they are often used to the PI controller. In addition, the PI controller can be attributed partly easy to operate, functional simplicity and robust performance. However, in nonlinear control systems, the parameter variations or uncertain parameters, if using PI traditional controller the system response maybe very hard to get a good control performance because, while operating systems  $K_p, K_i$  gain of traditional PI controller don't tune itself due to parameter variations of the nonlinear plants [17].

PID gain	Rise time	Over shot	Steady state error
$K_p$	↓↓	↑	↓
$K_i$	↓	↑	↓↓
$K_d$	—	↓↓	—

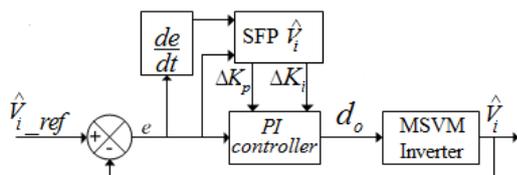
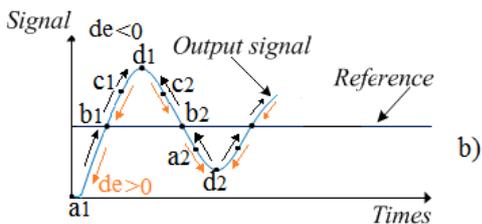


Fig. 5. Behavior of PID gain creasing [16] a) Rules SFP controller b) The PDV across the inverter bridge controller c).

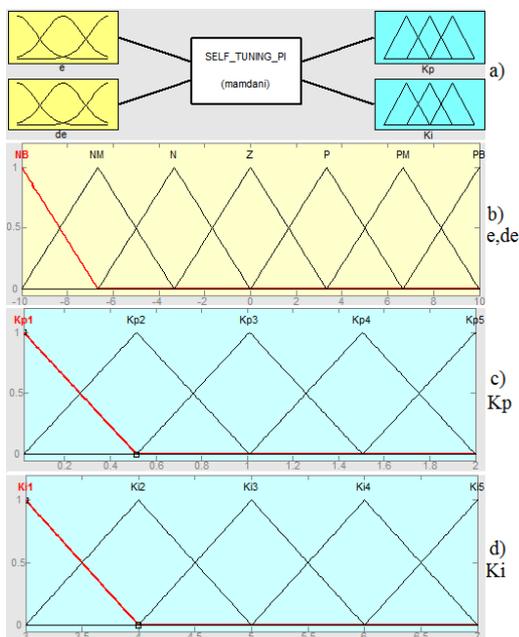


Fig. 6. Fuzzy inference with 2 input, 2 output a) Membership functions of input signal  $e, de$  b) Output signal  $K_p$  c),  $K_i$  d).

Therefore, this paper proposed control methods is SFP controller means that the two parameters  $K_p, K_i$  of conventional PI controller which gain of it are tuned by using fuzzy inference tuner (17) Fig. 5c) to improve quality control of systems such as: small error steady-state, less overshoot, decrease rise time and faster settling time. In addition, due to SFP has the advantage of adaptive, flexibility, high control precision, and robustness in speed control motor.

Following to the fuzzy structure, they include three blocks generally there are: fuzzification block, fuzzy inference engine that generates the fuzzy rules, defuzzification block [9]. All of membership function are chosen triangle, the aggregation are used max-min and defuzzification method are used centroid method. In Fig. 6a) there are two input signal  $e(t), de(t)$  and two output signal  $K_p, K_i$ . Where  $e(t)$  is the error between reference signal and the output,  $de(t)$  is the derivation of  $e(t)$

$$u(t) = K_p e(t) + K_i \int_0^t e(t) dt \quad (17)$$

where:  $u(t)$  is the signal control.

Base on the characteristics, specification of ZSI. Therefore, the linguistic variable levels of two input signal  $e(t), de(t)$  are assigned to seven levels, there are: NB: negative big; NM: negative middle; N: negative; Z: zero; P: positive; PM: positive middle; PB: positive big Fig. 6b). The linguistic variable levels of two output signal are assigned to five levels from small to large:  $K_{pj}$  and  $K_{ij} : j=1 \rightarrow 5$  on Fig. 6c),d).

In Fig.5a) shown that  $K_p$  play critical role on rise time,  $K_i$  plays this critical role on error steady-state and  $K_d$  only effects on over shot [16], [18]. From Fig.5b) at around  $a_1$ , the signal control should be tuned to increase dramatically in order to achieve fast rise time. So,  $K_p$  and  $K_i$  gain have to be tuned a big. Thus, the rule around  $a_1$ , are given:

If  $e$  is PB and  $de$  is Z, then  $K_p$  is  $K_{p5}$ ,  $K_i$  is  $K_{i5}$  Fig.7a),b). At around  $b_1$ , the signal control should be tuned small so less overshoot and small error steady-state. So,  $K_p$  and  $K_i$  gain have to be tuned a small. Therefore, the following fuzzy rule is given:

If  $e$  is Z and  $de$  is NB, then  $K_p$  is  $K_{p1}$ ,  $K_i$  is  $K_{i1}$  Fig.7a),b). Similar for around  $a_2, b_2, c_2, d_2$  fuzzy rule are given in Fig.7a),b). In Fig.5c) transfer function  $G_{V_{i-do}}$  in s-plane was given by [5].

$$G_{V_{i-do}}^{\wedge}(s) = \frac{\hat{V}_{i(s)}}{D_o(s)} \quad (18)$$

where  $\hat{V}_{i(s)}, D_o(s)$  are the PDV and shoot through duty in s-plane, respectively.

### III. SIMULATION AND EXPERIMENTAL RESULTS

#### A. Simulation Results

e\de	NB	NM	N	Z	P	PM	PB	e\de	NB	NM	N	Z	P	PM	PB
NB	Kp5	NB	Ki5												
NM	Kp4	NM	Ki3	Ki4	Ki4	Ki5	Ki4	Ki4	Ki3						
N	Kp3	N	Ki2	Ki3	Ki4	Ki5	Ki4	Ki3	Ki2						
Z	Kp1	Z	Ki1	Ki2	Ki3	Ki4	Ki3	Ki2	Ki1						
P	Kp3	P	Ki2	Ki3	Ki4	Ki5	Ki4	Ki3	Ki2						
PM	Kp4	PM	Ki3	Ki4	Ki4	Ki5	Ki4	Ki4	Ki3						
PB	Kp5	PB	Ki5												

Fig. 7. Rules of  $K_p$  a) And  $K_i$  b).

In order to verify the validity of the above analysis, using Matlab simulates a new algorithm control for DTC-MSVM control strategy for IM 5Hp in Fig.8d). In Fig.8d) shows response of DIV, time from 0 to 1s value of DIV is 500V, at time from 1s to 2s DIV decrease 10% (450V) after that at time from 2s to 3s DIV continue to decrease 10% (400V). The PDV and the dc-link voltage  $v_i$  decrease a little then immediately return to the steady-state (560V) is shown in Fig. 8a) and c). Especially, In Fig. 8c) show that PDV is controlled by using two algorithms, there are: self-tuning fuzzy PI and PI controller. These results was shown SFP

controller tracking a reference signal ( $\hat{V}_{i-ref} = 560V$ ) better than PI controller. These control methods also have the settling, overshoot and rise time less than PI controller when DIV is changed suddenly. Additionally, in Fig. 8b) duty  $d_o$  is also increase to the DIV sudden decrease at 1s, 2s. These simulation results are very appropriate with boost characteristics of ZSI.

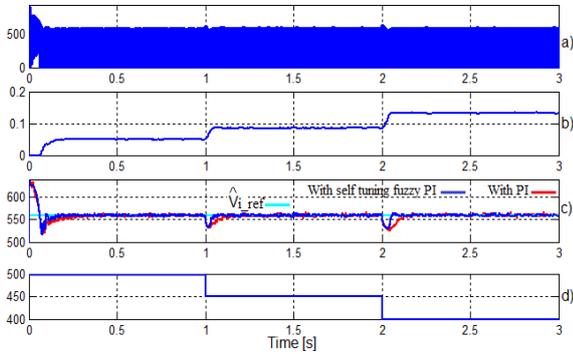


Fig. 8. The dc-link voltage  $v_i$  a) Duty  $d_o$  b) The PDV c) And DIV  $V_m$  d).

In Fig. 9a) when the DIV sudden decrease then the current waveform is unvaried. In addition, Fig. 9d) is shown low steady state electromagnetic torque  $T_e$  ripple and  $T_e$  is always tracking to load torque  $T_L$  when load torque sudden change. In Fig. 9b)  $THD\%$  is shown current's low total harmonic distortion  $THD\% = 3.58\%$ , speed motor is good steady-state show in Fig. 9c). Therefore, the PDV is controlled by SFP controller adapt to the DIV change, improves the transient response of PDV, increase robustness, applying good for speed control induction motor in the DTC-MSVM control strategy.

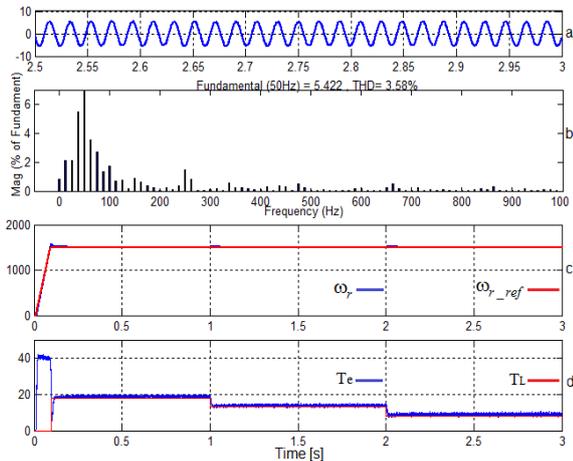


Fig. 9. The current a) THD% b) Speed motor c) Torque d).

### B. Experimental Results

In Fig. 11 is figure experiments of the speed control IM 1Hp base on the DTC-MSVM control strategy and applying a new control method for PDV are proposed. Application DSpace DS1103 communicate with Matlab2008, using controlDesk. V4.1 to display experiment results in Fig. 10 that they are shown to DIV sudden decrease at 1s, 2s Fig. 10b). So, the duty  $d_o$  increase Fig. 10a), speed motor is also tracking to  $\omega_r-ref$  very good when DIV  $V_{in}$  sudden change, given by in Fig. 10c). Line current is given by Fig. 10d). So, experiment results are given in Fig. 10 very appropriate simulation

results in Fig. 8 and Fig. 9.

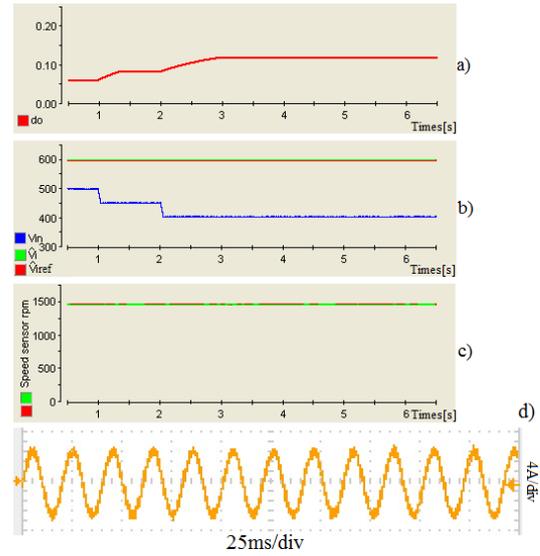


Fig.10. Duty  $d_o$  a) The peak dc-link voltage  $\hat{V}_i$ , the dc input voltage  $V_m$  b) And speed motor c) Line current d).

From simulation and experiment results show that characteristics of DTC-MSVM control strategy there are: when DIV decrease but PDV still hold voltage stabilization at 560V, so output voltage still stabilization. Additionally, DTC-MSVM control strategy is also to reduce the common voltage, not require dead-time protection short circuit at two switches any of the same phase leg increase robustness which it is the most focus to compare traditional DTC-SVM. Therefore, these characteristics are the most important reasons to choose DTC-MSVM control strategy for HEV applications.

TABLE I: PARAMETERS USED FOR SIMULATION AND EXPERIMENT OF DTC-MSVM

Parameter	Simulation	experiment
Z-source inductance ( $L_1$ and $L_2$ )(mH)	0.4	1.4
Z-source capacitance ( $C_1$ and $C_2$ )(mF)	0.5	0.25
Nominal power( $P_n$ )W, voltage( $V_n$ )(V)	3760;400	736;380
Frequency( $f_n$ )(Hz)	50	50
Stator( $R_s$ ); rotor( $R_r$ )resistance( $\Omega$ )	1.115;1.083	14.2;10
Stator( $L_s$ ); rotor( $L_r$ )inductance (H)	0.006;0.006	0.03;0.03
Magnetizing inductance( $L_m$ )(H)	0.2037	0.44
Switching frequency ( $f_{sf}$ )(kHz)	10	2
Pole pairs(p)	2	2
Inertia( $J_m$ )( $kg.m^2$ )	$2*10^{-2}$	$5.5*10^{-3}$
Friction factor( $B_m$ )(N.m.s)	$5.752*10^{-3}$	$1.5*10^{-3}$
DC-link peak voltage ( $\hat{V}_{i-ref}$ ) (V)	560	560
DC input voltage( $V_{in}$ )(V)	500,450,400	500,450,400
Speed motor ( $\omega_{r-ref}$ )(rpm)	1500	1490
load torque( $T_L$ )(N.m)	18,13,8	3,2,1



Fig. 11. The figure experiments.

## IV. CONCLUSION

With simulation and experimental results are given to verify the proposed a new algorithm to control the PDV in ZSI due to SFP controller by using fuzzy logic which it adapt to DIV sudden change, in order to improves transient response of PDV, to solve the problems of the output voltage stabilization in the inverter bridge. More importantly, this new algorithm is applied in closed loop speed control system of induction motor base on the DTC-MSVM control strategy with many exceptional features such as: fast torque response, low steady state torque ripple, increase accurate of speed motor, to increases robustness of speed motor control, enhances disturbance rejection and increase performance of the system. Therefor, the combination of SFP based control algorithm and DTC-MSVM control strategy is the best candidate for HEV applications.

## REFERENCES

- [1] I. Poh Chiang Loh, Member, D. M. Vilathgamuwa, I. Senior Member, Y. S. Lai, G. T. Chua, and I. Yunwei Li, Student Member, "Pulse-width modulation of z-source inverters," *IEEE Transactions on Power Electronics*, vol. 20, no. 6, pp. 1346–1355, 2005.
- [2] M. Olzwesky, "Z-source inverter for fuel cell vehicles," U.S. Department of Energy, Freedom CAR and Vehicles Technologies, EE-2G, 1000 Independence Avenue, SW, Washington, D.C. 20585-0121, 2005.
- [3] K. Holland, M. Shen, and F. Z. Peng, "Z-source inverter control for traction drive of fuel cell-battery hybrid vehicles," *Industry Applications Conference, Fourtieth IAS Annual Meeting*, vol. 3, no. 4, pp. 1651–1656, 2005.
- [4] X. Ding, Z. Qian, Shuitao, Y. B. Cui, and F. Peng, "A high-performance z-source inverter operating with small inductor at wide-range load," in *Applied Power Electronics Conference, APEC 2007 - Twenty Second Annual IEEE*, March 2007, pp. 615–620.
- [5] O. Ellabban, J. V. Mierlo, and P. Lataire, "Direct torque controlled space vector modulated induction motor fed by a z-source inverter for electric vehicles," in *Proceeding of the 2011 International Conference on Power Engineering, Energy and Electrical Drivers*, Malaga, Spain, May 2011.
- [6] M. Zeraoulia, M. E. H. Benbouzid, and D. Diallo, "Electric motor drive selection issues for hev propulsion systems: A comparative study," in *Vehicle Power and Propulsion, 2005 IEEE Conference*, Sept 2005, pp.1756–1764.
- [7] A. Haddoun, M. Benbouzid, D. Diallo, R. Abdessemed, J. Ghouili, and K. Srairi, "Comparative analysis of control techniques for efficiency improvement in electric vehicles," in *Vehicle Power and Propulsion Conference, VPPC*, Sept 2007, pp. 629–634.
- [8] M. Vasudevan and R. Arumugam, "New direct torque control scheme of induction motor for electric vehcles," in *5th Asian Control Conference*, 2004, pp.1377–1384.
- [9] X. Ding, Z. Qian, S. Yang, B. Cui, and F. Peng, "A direct dc-link boost voltage pid-like fuzzy control strategy in z-source inverter," in *Power Electronics Specialists Conference, PESC 2008. IEEE*, June 2008, pp. 405–411.
- [10] X. Ding, S. Yang, Z. Qian, B. Cui, and F. Peng, "A direct peak dc-link boost voltage control strategy in z-source inverter," in *Applied Power Electronics Conference, APEC 2007-Twenty Second Annual IEEE*, June 2007, pp. 648–653.
- [11] B. K. Bose, *Modern power Electronics and AC Drivers*. USA: Pearson Education, 2002.
- [12] T. Chun, Q. Tran, J. Ahn, and J. Lai, "Ac output voltage control with minimization of voltage stress across devices in the z-source inverter using modified svpwm," in *PESC 37th IEEE*, 2006, pp. 1–5.
- [13] Q. Tran, I. Tae.Won Chun, Member, J. Ahn, and I. Hong. Hee Lee, Member, "Algorithms for controlling both the dc boost and ac output voltage of z-source inverter," *IEEE Trans. Industrial Electronics*, vol. 54, no. 5, pp. 2745–2750, Mar. 2007.
- [14] I. Fang Zheng Peng, Senior Member, "Z-source inverter," *IEEE Trans.Industry Applications*, vol. 39, no. 2, pp. 990–997, Mar. 2003.
- [15] A. Khedher and M. F. Mimouni, "Sensorless-adaptive dtc of double star induction motor," *Energy Conversion and Management*51, vol. 51, no. 12, pp. 2878–2892, 2010.
- [16] N. Nahapetian, M. Motlagh, and M. Analoui, "Adaptive pid gain tuning using fuzzy logic and additional external performance index reference for controlling robot manipulator," in *International Conference on Advanced Computer Control*, Jan. 2009, pp. 448–452.
- [17] Zulfatman and M. F. Rahmat, "Application of self-tuning fuzzy pid controller on industrial hydraulic actuator using system identification approach," *International Journal on Smart Sensing and Intelligent Systems*, vol. 02, no. 02, pp. 246–261, 2009..
- [18] Z.-Y. Zhao, Member, I. Masayoshi Tomizuka, Member, and I. Satoru Isaka, Member, "Fuzzy gain scheduling of pid controllers," *IEEE Transactions on Systems, Man, and Cybernetics*, vol. 23, no. 5, pp. 1392–1398, 1993.